SODIUM-SULFUR BATTERY FLIGHT EXPERIMENT DEFINITION STUDY

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Summary

The need for high power space systems is anticipated within the next 10 to 20 years. Examples are the Space Station, co-orbiting platforms, geostationary orbit (GEO) platforms, and space-based radar satellites and some classified high power missions. Sodium-sulfur (Na-S) batteries have been identified as the most likely successor to nickel-hydrogen (Ni-H₂) batteries for space applications. One advantage of the Na-S battery system is that the useable specific energy is two to three times that of Ni-H₂ batteries. This represents significant launch cost savings or increased payload mass capabilities. Na-S batteries support NASA OAST's proposed Civil Space Technology Initiative goal of a factor of two improvement in spacecraft power system performance, as well as the proposed Spacecraft 2000 initiative.

The Na–S battery operates at between 300 and 400 $^{\circ}$ C, using liquid sodium and sulfur/polysulfide electrodes and solid ceramic electrolyte [1-3]. The transport of the electrode materials to the surface of the electrolyte is through wicking/capillary forces. These critical transport functions must be demonstrated under actual microgravity conditions before Na–S batteries can be confidently utilized in space.

Ford Aerospace Corporation, under contract to NASA Lewis Research Center, is currently working on the Na-S battery space flight experiment definition study. The objective is to design the experiment that will demonstrate operation of the Na-S battery/cell in the space environment, with particular emphasis on evaluation of microgravity effects. Experimental payload definitions have been completed and preliminary designs of the experiment have been defined.

Introduction

The Na-S battery cell, pioneered by Ford Motor Co., is seen as one of the most attractive battery systems for spacecraft power systems. The

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primary advantage of this system is its high energy density, which can reach 150 W h kg⁻¹ at C-rate discharge at the cell level. The Na-S battery offers a combination of system level advantages:

- mass and volume effectiveness;
- high round-trip efficiency;
- heat rejection at high temperature;
- simplicity of battery integration;
- competitive acquisition costs.

Nominal Na–S cell operating parameters are shown and compared with typical Ni–Cd and Ni–H₂ cell data in Table 1. Unusual performance features for the Na–S cells are the high cell operating voltages, high round-trip efficiency, and high operating temperature which minimizes the radiator area and cost. Potential cost savings are illustrated in Table 2. It is obvious that the battery mass savings are translated into spacecraft launch cost savings or payload capability increase. Using Ni–H₂ systems as a reference, it can save in launch costs from 1.1 to 1.7 M\$ kW⁻¹ for the GEO missions and 0.2 - 0.4 M\$ kW⁻¹ for the LEO missions. For example, a 2.5 kW aerospace Na–S battery concept design weighs 31.8 kg, while a 0.5 kW Ni–H₂ battery weighs 30.5 kg.

The Na-S battery is a particularly good energy storage system for high power satellite missions. A parametric study comparing the operational storage candidates for a 75 kW satellite mission has been performed by Ford Aerospace and the results are shown in Table 3 [4]. The Na-S battery looks the most favorable with regard to the other storage systems.

The Na-S battery cells operate at between 300 and 400 °C. The liquid electrode materials rely on the wicking actions for transport to, and from, the electrolyte interface to support routine cyclic operation. Current

Battery system	Condi- tion	Average cell voltage (V)		Round-trip efficiency	Discharge dissipation	Operating temperature	Typical DOD
		Charge	Discharge	(%)	(kW_t/kW_e)	(°C)	(%)
Ni/Cd	GEO	1.43	1.22	80	0.18	0 - 20	45 - 60
	LEO	1.45	1.23	80	0.17	0 - 20	15 - 22
Ni/H ₂	GEO	1.45	1.25	80	0.20	0 - 20	68 - 80
(IPV)	LEO	1.47	1.27	80	0.18	0 - 20	28 - 40
Ni/H_2	GEO	1.45	1.26	82	0.19	0 - 20	68 - 80
(bipolar)	LEO	1.46	1.28	82	0.27	0 - 20	28 - 40
Na/S	GEO	2.10	1.83	87	0.18	300 - 400	50 - 80
	LEO	2 .15	1.80	84	0.21	300 - 400	35 - 50

Space battery operating parameter comparison

TABLE 1

Battery system	Condi- tion	Mass performance (kg kW ⁻¹)	Volume performance	Cost $vs. Ni/H_2$ (M\$ kW ⁻¹)		Life (years)
			$(l kW^{-1})$	Prod	Launch	() ()
Ni/Cd	GEO	55 - 90	30 - 55	1.1	+1.0 - 1.5	5 - 7
	LEO	70 - 140	40 - 85	1.6	+0.3 - 0.5	5 - 5
Ni/H ₂	GEO	35 - 60	60 - 120	1	0	10 - 15+
(IPV)	LEO	35 - 70	60 - 150	1	0	5 - 8
Ni/H2	GEO	35 - 60	25 - 45	1.2	0	10 - 15+
(Bipolar)	LEO	35 - 70	25 - 55	1.2	0	5 - 8
Na/S	GEO	13 - 25	40 - 120	1.2	-1.1 - 1.7	5 - (a)
	LEO	11 - 20	30 - 85	1.2	-0.2 - 0.4	$1 \cdot (\mathbf{a})$

TABLE 2 Sodium/sulfur batteries offer spacecraft mass savings

(a)Requires demonstration.

TABLE 3

Energy storage system options comparison

Parameter	RFC H ₂ -O ₂	RFC H ₂ -O ₂	BIPOL Ni-H2	IPV Ni–H2	Ni–Cd	Na-S	Fly wheel
	2 - 2						<u></u>
Round trip efficiency (%)	55	60	77	75	75	82	82
Depth-of-discharge (%) ^a	38	38	38	38	20	38	38
Mass (kg)	2100	2500	3300	4100	9500	1500	4200 ^b
Volume (m ³)	9.3	9.9	2.5	6.6	5.2	1.9	4.0 ^b
Waste heat/cycle (kW h)	42	34	15	17	17	11	11
Eclipse heat rejection (kW)	57	55	17	18	17	17	9
Temperature (°C)	80	80	10	10	10	350	35
Charge power requirement (kW)	98	90	74	76	76	66	66

^aIn all cases except Ni-Cd controlled by one orbit half power requirement following a full power eclipse.

^bExclusive of containment.

developmental space cells have been designed to have adequate wicking, but this critical function must be demonstrated under actual orbital microgravity conditions before Na-S batteries can be confidently applied in space. The primary objective of the Ford Aerospace study is to define the specific experimental design required for successful demonstration of the Na-S battery/cell under space environments.

Cell operations and selections

Na–S cells, as shown in Fig. 1, utilize a solid ceramic electrolyte, known as β'' -alumina, to separate anode (sodium) and cathode (sulfur/sodium polysulfide) reactants and to provide a conductive path for sodium ions during operation. The transport of the electrode materials to the surface of the electrolyte is through wicking/capillary forces. A metal protection tube limits the flow of sodium into the reaction zone, thus providing for safe operation of the cell. Since only small amounts of the sodium are available for reaction, a quick, explosive reaction cannot occur, even in the case of a broken electrolyte tube. The sulfur is contained in the outer part of the cell, imbedded in a carbon fiber mat. The carbon fiber mat improves the electrical conduction path for the sulfur electrode.



At the cell operating temperature, the reactants are in the liquid state. During discharge of the cell, the sodium splits into positive ions, which are transported across the electrolyte, and negative electrons, which are carried up by the current collector to the external circuit. Once the sodium ions are transported across the ceramic electrolyte, they join with the sulfur to form a sodium polysulfide (Na_2S_5). As the cell is further discharged, the Na_2S_5 reacts with sodium to form other sodium polysulfides such as Na_2S_4 and Na_2S_3 . Charging the cell results in the opposite reactions, with the sodium polysulfides being broken down into sodium ions and sulfur. The sodium ions are then transported back across the electrolyte to the sodium electrode.

The proposed flight experiment cells, which are rated 40 A h, are derived from the Ford Aerospace baseline SATBAT-2 cells. The physical



Fig. 2. Ford Aerospace Na-S cells.

characteristics of the cells are summarized as follows, and typical 40 A h cells are shown in Fig. 2.

Cell capacity (A h)	40.0
Outer diameter (cm)	3.6
Cell length (cm)	23.0
Cell mass (g)	519.0

Flight experiment justifications and objectives

Na–S cells differ from most batteries in that they contain molten anodic and cathodic reactants. The ability of the Na–S cells to charge and discharge efficiently is critically dependent upon the favorable spatial distribution of the fluid reactants in regard to their interface with the solid β "-alumina ceramic electrolyte. Fluid motion and reactant morphology are particularly critical for Na–S cell operation, since the sulfur/sodium polysulfide catholyte reactants form three immiscible phases during recharge, two of which are non-conductive: molten sulfur, void volume, and Na₂S₅. Should an unfavorable distribution occur, a blocking layer could develop and restrict cell operation.

Terrestrial cell designs incorporate preferential wetting, capillarity, and/or graded resistance within the sulfur electrode to maintain efficient operation. Such cells have been developed to operate effectively at high rate and to yield high specific energy and specific power. However, the characteristics of Na-S cells under microgravity conditions are unknown because of the uncertain role of gravity in controlling the distribution and consolidation of the separate reactant phases. These effects can only be determined by testing in orbit with 3-axis stabilized spacecraft, because it is not possible to simulate low gravity conditions for sufficiently long times to represent cycling or the large equilibration time constraints associated with the sluggish fluids.

The main purpose of the Na-S battery/cell flight experiment is to validate the application of Na-S battery technology to space power applications. The principal objective of the flight experiment definition study is to design an experiment that will demonstrate operation of the battery/cells under space environments with particular emphasis on evaluation of microgravity effects which are specially critical for 3-axis stabilized spacecrafts. These can be categorized as follows:

(i) to evaluate cell charge and discharge characteristics as affected by the fluid reactant distributions;

(ii) to determine reactant distributions under microgravity conditions;

- (iii) to understand current and thermal distributions within the cells;
- (iv) to evaluate freeze/thaw effects;
- (v) to evaluate multi-cell early LEO (Low Earth Orbit) cycle life.

The approach is to select only those tests that are critical and expected to differ under microgravity conditions. Spin stabilized satellite batteries can be tested on the ground; thus a test to simulate this application in space is not needed. Warm launch has an advantage that the cells in space will require less energy and time to heat up from the warm launch temperature to its final operating temperature. However, the demonstration of the cell survivability to the launch environments can be confirmed on the ground by test, followed by electrical cyclic testings. Therefore, the warm launch test need not be included in the experiment.

Description of proposed experiments

Five tests have been identified in the Na-S battery flight experiment definition study to meet the above objectives. Each of these tests will be summarized in the following sections.

(i) Cell characterization test

- (ii) Reactant distribution test
- (iii) Current/temperature distribution test
- (iv) Freeze/thaw test
- (v) Multi-cell LEO cycle test

The test cells will be Ford Aerospace baseline 40 A h cells except Test (iii) cells, which will be specially instrumented with extra thermocouples and voltage probes.

Our general testing philosophy is to have most of the space cells evaluated under various conditions on the ground prior to launch, in space, and after cells are brought back to earth, to provide before-during-after data comparison. Additional control cells will be assigned to an identical ground test to provide additional comparative data base.

(i) Cell characterization test

Na-S cells will be evaluated under various test conditions in space at two temperatures, 275 °C and 350 °C. Once orbit has been stabilized, the cells will be heated to operating temperatures and the test sequence performed. The charge/discharge cycle variables have been established to cover a sufficiently wide range of parameters to address a majority of anticipated space applications. Pulse loads will be imposed during the discharge. Each cell will be instrumented with power leads, voltage sense leads, and a thermocouple pair, all which will penetrate the thermal insulation barrier for connection to ambient temperature connector panels. During the charge/discharge cycle, each cell voltage will be periodically measured.

(ii) Reactant distribution test

After completion of Test (i), the cells will be discharged into their 1-phase region and placed on open circuit to determine their state-of-charge accurately. Each state of charge of the cell will be adjusted to a composition ranging from Na_2S_3 to Na_2S_5 .

(iii) Current/temperature distribution test

This test will continuously determine the spatial variations of electrode reactions and current densities within the sulfur electrode throughout the electrical cycles, while being operated under microgravity conditions. This information will support analysis and assessment of test results of Tests (i) and (ii), and will direct possible modifications to the sulfur electrode design should that prove necessary.

The distribution of internal current densities and electrode reactions will be measured continuously during the electrical cycles by measuring the electrodes small ohmic losses. Specially instrumented cells will be fabricated to incorporate a multitude of voltage probes on the positive current collector. In addition to the external thermocouples located at the top, middle, and bottom of the cell container, internal thermocouples on the inside electrolyte tube wall will also be installed at respective locations to measure the temperature gradients. Three sets of voltage probes will be used to provide information about circumferential uniformity.

(iv) Freeze/thaw test

Cells will be evaluated for the freeze/thaw cycles. They will be initially heated to operating temperature and evaluated electrically, followed by several freeze/thaw cycles. On the last day of the flight experiment, cells will be again evaluated electrically to determine the effects of freeze/thaw under microgravity conditions. The cells will be cooled for re-entry.

(v) Multi-cell LEO cycle test

Na-S cells will be series connected and evaluated in the 90 min orbit regime. Cells will be cycled at a high rate discharge for 36 min followed by

a charge for 54 min. It is almost impossible to evaluate the life cycle of the Na-S cells in such a short experimental duration. However, the proposed LEO cycle will provide an early life, real time LEO operational experience and will demonstrate the multi-cell operation. Information obtained will be valuable for full size battery scaling-up.

System implementation and carrier options

A variety of payload carriers, shown in Fig. 3, including Middeck Modular Locker, Get Away Special, Hitchhiker G, and Hitchhiker M have been reviewed [5]. Concerns such as electrical power, mass load/structure, and mounting orientation have been considered as factors for carrier selections. From the preliminary design of the five tests, the total weight of the enclosures, batteries, and support equipments is estimated to be a total of less than 100 lb. The experiment will occupy a space approximately 3.0 ft. \times 3.0 ft. \times 1.5 ft.



Fig. 3. Payload carrier options.

Conclusions

Na-S batteries have been identified as the most likely successor to space Ni-H₂ or Ni-Cd batteries, primarily due to a mass reduction by a factor of 2 - 3 over Ni-H₂ and by a factor of 4 over Ni-Cd. This leads to major launch cost reductions or payload mass improvements. Na-S batteries support NASA OAST's proposed Civil Space Technology Initiative goal of a factor of two improvement in spacecraft 2000 initiative. Since Ni-H₂ and Ni-Cd batteries have been space flight proven, it is essential to have a flight experiment to establish a national space technology base to demonstrate the operation of the Na-S battery in space applications.

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References

- 1 R. W. Minck and C. R. Halbach, Characteristics of sodium-sulfur cells for diverse applications, Proc. 17th IECEC, 1982, p. 557.
- 2 H. L. Haskins, M. L. McClanahan and R. W. Minck, Sodium-sulfur cells for highpower spacecraft batteries, Proc. 18th IECEC, 1983, p. 1465.
- 3 D. M. Allen, Sodium-sulfur satellite batteries: cell test results and development plans, Proc. 19th IECEC, 1984, p. 163.
 4 C. W. Koehler, A. Z. Applewhite, A. M. Hall and P. G. Russell, Bipolar nickel-hydro-
- gen battery development, Proc. 20th IECEC, 1985.
- 5 STS Investigators Guide, available from NASA/MSFC, Marshall Space Flight Center, AL 35812, U.S.A.